

523
NPSEC-94-002

NAVAL POSTGRADUATE SCHOOL

Monterey, California



PERFORMANCE COMPARISON AN/FRD-10 vs. PUSHER

by

Wilbur R. Vincent
Richard W. Adler

February 1994

Approved for public release; distribution unlimited.

FEDDOCS
D 208.14/2
NPS-EC-94-002

Security Group Command
Nebraska Ave., NW
ngton, DC 20393-5220

Naval Postgraduate School
Monterey, California 93943-5000

Rear Admiral T. A. Mercer
Superintendent

H. Shull
Provost

This report was funded by the Naval Security Group Command.

Reproduction of all or part of this report is authorized.

This report was prepared by:

Computer Engineering

REPORT DOCUMENTATION PAGE

Form Approved

OMB No. 0704-0186

Public reporting burden for this collection of information is estimated to average 1 hour per response, including the time for reviewing instructions, searching existing data sources, gathering and maintaining the data needed, and completing and reviewing the collection of information. Send comments regarding this burden estimate or any other aspect of this collection of information, including suggestions for reducing this burden, to Washington Headquarters Services, Directorate for Information Operations and Reports, 1215 Jefferson Davis Highway, Suite 1204, Arlington, VA 22202-4302, and to the Office of Management and Budget, Paperwork Reduction Project (0704-0186), Washington, DC 20503.

1. AGENCY USE ONLY (Leave blank)

2. REPORT DATE

February 1995

3. REPORT TYPE AND DATES COVERED

Interim Report

4. TITLE AND SUBTITLE

PERFORMANCE COMPARISON
AN/FRD-10 vs. PUSHER

5. FUNDING NUMBERS

6. AUTHOR(S)

Wilbur R. Vincent and Richard W. Adler

7. PERFORMING ORGANIZATION NAME(S) AND ADDRESS(ES)

Naval Postgraduate School
Monterey, CA 93943-50008. PERFORMING ORGANIZATION
REPORT NUMBER

NPSEC-94-002

9. SPONSORING/MONITORING AGENCY NAME(S) AND ADDRESS(ES)

Naval Security Group Command
Code G43
3801 Nebraska Avenue NW
Washington DC 20393-522010. SPONSORING/MONITORING
AGENCY REPORT NUMBER

11. SUPPLEMENTARY NOTES

The views expressed in this report are those of the authors and do not reflect the official policy or position of the Department of Defense or the United States Government.

12a. DISTRIBUTION/AVAILABILITY STATEMENT

Approved for public release;
distribution unlimited.

12b. DISTRIBUTION CODE

13. ABSTRACT (Maximum 200 words)

The possibility of replacing some of the AN/FRD-10 Circular Disposed Antenna Array (CDAA) facilities with lower cost PUSHER type of CDAA is an option available to planners. It is generally assumed that the ability of the PUSHER to receive signals of interest (SOI) is only slightly less than that of the larger AN/FRD-10 and AN/FLR-9 types of CDAA. However, no specific analysis of the actual difference in performance is known to exist. This report provides a preliminary performance analysis of the two types of facilities.

Detailed performance-related measurements have been made at a number of AN/FRD-10 CDAA sites. These measurements were made as a part of the U.S. Navy's Signal-to-Noise-Enhancement Program (SNEP). The objective of the SNEP is to identify and mitigate all factors that degrade the ability of receiving sites to receive SOI and process data from them. Similar measurements have also been made at PUSHER sites, although complete data is available from only a single PUSHER site. This report uses data accumulated from the AN/FRD-10 sites and from one measured PUSHER site to examine the differences in their ability to receive SOI.

The performance Evaluation Technique (PET) developed by the Naval Postgraduate School was used to evaluate the performance of each kind of CDAA. To simplify this initial analysis, the assumption was made that an AN/FRD-10 site containing an RFSS type of RF switch would be replaced with a PUSHER. Only the technical properties of the two types of CDAA were considered. The additional adverse impact of internal and external sources of man-made noise on performance was not included. It was assumed that the impact of EMI would be the same for both types of systems. In addition, the effect of nighttime overloading and saturation of the RF-distribution systems (RFD) from the relatively high levels of total signal power collected by the antenna elements were not considered in this preliminary analysis.

14. SUBJECT TERMS

EMI/RFI, high frequency direction finding, CDAA, signal to noise enhancement

15. NUMBER OF PAGES

project 17

16. PRICE CODE

17. SECURITY CLASSIFICATION

OF REPORT
UNCLASSIFIED

18. SECURITY CLASSIFICATION

OF THIS PAGE
UNCLASSIFIED

19. SECURITY CLASSIFICATION

OF ABSTRACT
UNCLASSIFIED

20. LIMITATION OF ABSTRACT

SAR

INTRODUCTION

The possibility of replacing some the AN/FRD-10 Circular Disposed Antenna Array (CDAA) facilities with the lower cost PUSHER type of CDAA is an option available to planners. It is generally assumed that the ability of the PUSHER to receive signals of interest (SOI) is only slightly less than that of the larger AN/FRD-10 and AN/FLR-9 types of CDAA. However, no specific analysis of the actual difference in performance is known to exist. This memorandum provides a preliminary performance analysis of the two types of facilities.

Detailed performance-related measurements have been made at a number of AN/FRD-10 CDAA sites. These measurements were made as a part of the U.S. Navy's Signal-To-Noise-Enhancement Program (SNEP). The objective of the SNEP is to identify and mitigate all factors that degrade the ability of receiving sites to receive SOI and process data from them. Similar measurements have also been made at PUSHER sites, although complete data is available from only a single PUSHER site. This memorandum uses data accumulated from the AN/FRD-10 sites and from the one measured PUSHER site to examine the differences in their ability to receive SOI.

The Performance Evaluation Technique (PET) developed by the Naval Postgraduate School was used to evaluate the performance of each kind of CDAA. To simplify this initial analysis, the assumption was made that an AN/FRD-10 site containing an RFSS type of RF switch would be replaced with a PUSHER. Only the technical properties of the two types of CDAA were considered. The additional adverse impact of internal and external sources of man-made noise on performance was not included. It was assumed that the impact of EMI would be the same for both types of systems. In addition, the effect of nighttime overloading and saturation of the RF-distribution systems (RFD) from the relatively high levels of total signal power collected by the antenna elements were not considered in this preliminary analysis.

BASIS FOR ANALYSIS

Measured gains and losses of the RFD of a typical AN/FRD-10 CDAA and a PUSHER are provided in Table 1. Values of loss are provided in increments of 2.5 MHz over the frequency band of 2 to 30 MHz. These values are provided in Columns 2 and 3 of the table. Other differences between the two systems must also be taken into account. For example, the antenna gain of the PUSHER is estimated to be about 3-dB less than that of the AN/FRD-10. This is shown in Column 4. The PUSHER uses RG-8 coaxial cable from each element to its center hut whereas the AN/FRD-10 uses large low-loss cable. The calculated difference in cable loss is shown in Column 5. The total RF loss of the PUSHER is shown in Column 6.

Table 1
 Signal Loss Values

Frequency MHz	AN/FRD-10 RFD Loss dB	PUSHER RFD Loss dB	PUSHER Antenna Loss dB	PUSHER Cable Loss dB	PUSHER Total Loss dB
2.5	4.4	19.0	3.0	1.0	23.0
5.0	3.6	14.0	3.0	1.0	21.0
7.5	3.8	7.0	3.0	1.0	11.0
10.0	0.0	11.0	3.0	1.0	15.0
12.5	0.0	13.0	3.0	2.0	18.0
15.0	0.0	8.0	3.0	2.0	14.0
17.5	0.0	22.0	3.0	2.0	27.0
20.0	0.0	10.0	3.0	2.0	15.0
22.5	1.1	22.0	3.0	3.0	28.0
25.0	1.5	17.0	3.0	3.0	23.0
27.5	2.3	11.0	3.0	3.0	17.0
30.0	0.5	22.0	3.0	3.0	28.0

The noise floor of active elements of the RFD in both the AN/FRD-10 and the PUSHER determine the lowest level signal that can be received. The noise floors of the RFD of both types of systems has been measured using a 3-kHz-wide gaussian-shaped measurement bandwidth. The values of noise floor for each system are provided in Table 2.

Frequency MHz	AN/FRD-10 Noise Floor dBm	PUSHER Noise Floor dBm
2.5	-124	-116
5	-124	-116
7.5	-124	-116
10	-124	-116
12.5	-124	-116
15	-124	-116
17.5	-124	-116
20	-124	-116
22.5	-124	-116
25	-124	-116
27.5	-124	-116
30	-124	-116

Table 2
Noise Floor

PERFORMANCE EVALUATION

Signal loss between the antenna and a receiver decreases the amplitude of signals provided to that receiver. Signals that fall below the RFD noise floor measured at the input to a receiver will not be detected. These factors are routinely measured by SNEP teams to identify operational problems within a CDAA site. Data accumulated over a number of years was used as the basis for the comparison of the PUSHER to the AN/FRD-10 CDAA.

The signal loss and noise floor values in Tables 1 and 2 provide the basis to compare the underlying capabilities of each type of CDAA to receive SOI. A specific type of SOI located within the primary coverage zone of a mid-latitude site was selected for the analysis of the performance of each type of CDAA. The SOI used a transmitter power of 1 kW and a dipole antenna. It was assumed that the SOI employed modulation that could be detected by a receiver at a 0-dB (S+N)/N. A log-normal amplitude distribution was used for the comparison.

Figure 1 shows the result of the comparison. Row 1 (blue) of the presentation shows the performance level of the AN/FRD-10. The small decrease in performance below 8 MHz was the result of an older model low-band multicoupler. The replacement of this multicoupler with a newer model will improve the low-band performance capability of that system.

Row 2 (yellow) shows the effect of only the RFD signal loss on the ability of the PUSHER to receive the same SOI. RFD loss seriously degrades the ability of this type of system to receive SOI. This result indicates that every effort should be made to decrease the RFD signal loss in existing and future PUSHER systems.

Row 3 (red) shows the overall performance of a complete PUSHER system. The loss of the RG-8 coaxial cable from the PUSHER's antenna elements to its center hut is added to the RFD loss in this line. A cable length of 100 feet was used which may be shorter than that used in most PUSHER installations. The exact cable lengths were not available at the time of this preliminary analysis.

The results indicate that a PUSHER installation side-by-side with an AN/FRD-10 will receive less than half the number of SOI received by the AN/FRD-10. This assumption assumes that both systems have the same internal and external man-made noise levels. The susceptibility of the two systems to man-made noise problems is not considered in this preliminary evaluation.

PERFORMANCE COMPARISON

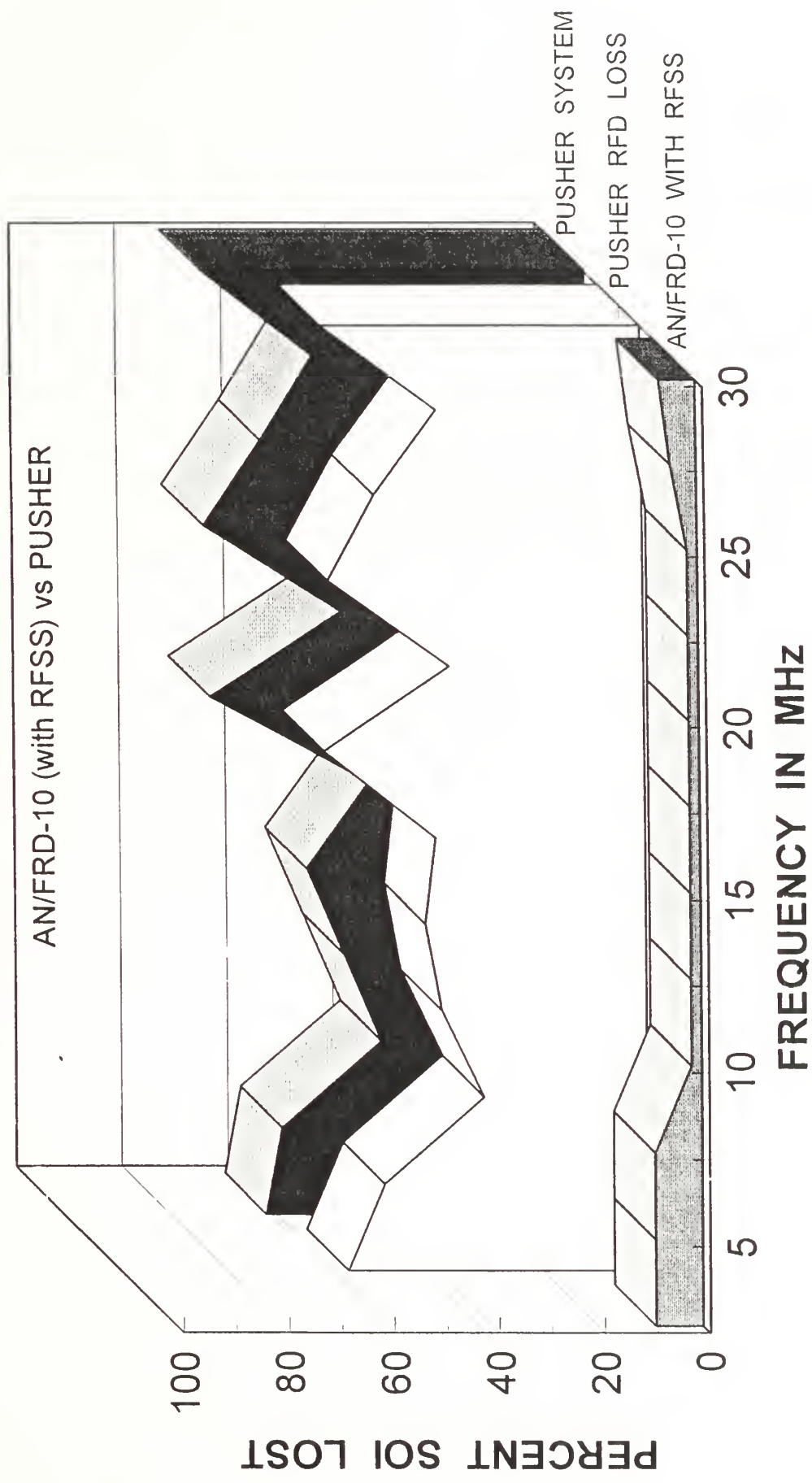


Figure 1
Performance Comparison

Unfortunately, the SOI missed by the PUSHER will not be a random sampling of the incoming signals. The lost SOI will be those below a specific field strength level. SOI that are very strong in amplitude will be received equally well by both CDAA systems. Since each kind of SOI will be received with a distribution of amplitudes ranging from modest down to very weak, a receiver using the PUSHER will not detect many of the SOI that are collected by its antenna. There is no class of SOI that the PUSHER will receive as well or better than the AN/FRD-10.

The data base available for the analysis of the performance of the AN/FRD-10 CDAA is extensive; however the data base for the PUSHER is limited. While the data used for the analysis of the PUSHER CDAA appears to be normal and in general agreement with limited samples of data from other PUSHER sites, more data from additional sites would be useful.

CONCLUSIONS

The initial comparison of the performance of the AN/FRD-10 CDAA with a PUSHER CDAA has provided rather surprising results. These results do not agree with the conventional view of the two systems which suggest that only small antenna-related differences in performance exist. The following summarize the findings and conclusions.

- Excessive signal loss and excessive noise floor of the RFD of the PUSHER CDAA are major reasons for the large difference in performance of the PUSHER when compared to an AN/FRD-10 CDAA. These two factors allow the PUSHER to receive only about one half as many SOI as an AN/FRD-10.
- The use of RG-8 cable to carry signals from the PUSHER antenna elements to the center hut adds to the RFD loss and further degrades its ability to provide detectable signals to receiving systems. This factor can be corrected by changing the antenna element cables to a low-loss type of cable.
- The smaller antenna aperture of the PUSHER over the AN/FRD-10 also adds to its lower level of performance, however this factor is of lower importance than the signal loss and noise floor factors.
- The correction of the signal loss and noise floor problems in a PUSHER will require a major and costly redesign of the RFD system for that type of CDAA.

INITIAL DISTRIBUTION LIST

	No. Copies
1. Defense Technical Information Center Cameron Station Alexandria, VA 22304-6145	1
2. Dudley Knox Library, Code 52 Naval Postgraduate School Monterey, CA 93943-5002	2
3. Chairman, Code EC Department of Electrical and Computer Engineering Naval Postgraduate School 833 Dyer Road, Room 437 Monterey, CA 93943-5121	1
4. Professor Richard W. Adler, Code EC/Ab Department of Electrical and Computer Engineering Naval Postgraduate School 833 Dyer Road, Room 437 Monterey, CA 93943-5121	4
5. Professor Wilbur R. Vincent, Code EC/Ab Department of Electrical and Computer Engineering Naval Postgraduate School 833 Dyer Road, Room 437 Monterey, CA 93943-5121	2
6. Mr. Chris Adams ManTech 6593 Commerce Court Gainesville, VA 22065	1
7. Mr. Jeff Artman NESSEC 3801 Nebraska Avenue NW Washington DC 20393	1
8. Ms. Ruth A. Bates 7642A Murphy Loop Ft. Meade, MD 20755	1

	No. Copies
9. Mr. Mark W. Beighey ManTech Field Engineering Corp. Box 721, 751 MI BN APO San Francisco 96271	1
10. Mr. Roy Bergeron ERA 1595 Spring Hill Road Vienna, VA 22180	1
11. Mr. Norman R. Berabe NESSEC 3801 Nebraska Avenue NW Washington DC 20393	1
12. Ms. Anne B. G. Bilgiban USA INSCOM MSA-V EAQ Building 160 MS 26 Vint Hill Farms Station Warrenton, VA 22186-5160	1
13. Mr. Bryan Bollinger NSA/R-521 9800 Savage Road Ft. Meade, MD 20755-6000	1
14. Mr. Arthur Carter NSA/R-521 9800 Savage Road Ft. Meade, MD 20755-6000	1
15. Mr. John Chalupski NESSEC 3801 Nebraska Avenue NW Washington DC 20393	1
16. Mr. Donald Clark Naval Security Group, Code GX 3801 Nebraska Avenue NW Washington DC 20393	1

	No. Copies
17. Mr. Gene Cummins, Jr. US Tower Services 5263 Agro Drive Frederick, MD 21701	1
18. MCMS F. Cunningham NSA, T2424 Ft. Meade, MD 20755	1
19. Mr. Bruce Damon Naval Security Group, Code GX 3801 Nebraska Avenue NW Washington DC 20393	1
20. Mr. Roy Dossat SPAWARS, Code PMW 144-3 NC1 3E52 Arlington, VA 20363	1
21. Mr. Jim Engels NESSEC, Code 0411 3801 Nebraska Avenue NW Washington DC 20393	1
22. Ms. Pamela Guardabascio NESSEC 3801 Nebraska Avenue NW Washington DC 20393	1
23. Mr. George Hagn SRI International 1611 N. Kent Street Arlington, VA 22209	1
24. Mr. Clyde Hartcock 1715 15th Street NW Washington DC 20009	1
25. Mr. Lee M. Jackson NCCOSC NRAD 825 1918 Via Las Palmas #17 National City, CA 91950	1

	No. Copies
26. Mr. Leo Jonas USAF ESC/LEMP San Antonio, TX 78243-5000	1
27. M. Jordan US Army INSCOM/MSA-V, Bldg 160 Vint Hill Farms Warrenton, VA 22186	1
28. Mr. Steve Kelly NESSEC, Code 0411A 3801 Nebraska Avenue NW Washington DC 20393-5210	1
29. S. Kobashigawa NEEACT PAC Box 130 Pearl Harbor, HI 96860-5170	1
30. Mr. Brian I. Kutara NEEACT PAC Box 130 Pearl Harbor, HI 96860-5170	1
31. CDR Gus Lott Naval Security Group, Code GX 3801 Nebraska Avenue NW Washington DC 20393	1
32. Mr. Thomas L. Lutz COMSPAWARSSYSCOM CMW 169-22 Washington DC 20636-5100	1
33. Mr. Stephen Masison NESSEC, Code 0412F 2801 Nebraska Avenue NW Washington DC 20393	1
34. Mr. George F. Munsch 160-CR-375 San Antonio, TX 79253	1

	No. Copies
35. Mr. Tom Murdock ERA 1595 Spring Hill Road Vienna, VA 22180	1
36. Mr. Hugh Myers NEEACT PAC Box 130 Pearl Harbor, HI 96860-5170	1
37. Mr. Hank Orejnelia Sanders Associates 95 Canal Street Nashua, NH 03061-2004	1
38. Mr. Charles K. Orthman NESSEC, Code 0412D 3801 Nebraska Avenue NW Washington DC 20393	1
39. LCDR Andrew Parker US Naval Academy Department of Electrical Engineering Annapolis, MD 21402	1
40. Ms. Jane Perry 1921 Hopefield Road Silver Springs, MD 20904	1
41. M. Robert M. Perry, Code EC/Ab Naval Postgraduate School 833 Dyer Road, Room 437 Monterey, CA 93943-5121	1
42. Mr. Marc Poussard 6 Dudley Court Bethesda, MD 20814	1
43. Ms. Tamara Preston-Boyd Naval Research Laboratory, Code 5326.1 455 Overlook Avenue SW Washington DC 20375-5000	1

	No. Copies
44. Mr. Art Reid 1177 Bolinger Road Littlestown, PA 17340	1
45. Mr. Miguel J. Sanchez Naval Security Group, Code G042 Ft. Meade, MD 20755-6000	1
46. Captain Brian Schumanski US Marine Corps Quantico, VA 22134-5080	1
47. Mr. Richard Sharp NESEA, Code 2133 St. Inigoes, MD 20684	1
48. Mr. Brian Skimmons Naval Security Group, Code GX 3801 Nebraska Avenue NW Washington DC 20393	1
49. Mr. Miles Terayama NISE West Hawaii Box 130 Pearl Harbor, HI 96860-5170	1
50. W. M. Wichman Lockheed Sanders, Inc. PTP1-2850 P.O. Box 868 Nashua, NH 03061-0686	1
51. C. Yashusa NEEACT PAC Box 130 Pearl Harbor, HI 96860-5170	1
52. LT D. Streight NAVCOMTEL STA SD NAVSECGRUDEPT/NRRF 500 Silver Strand Blvd. Imperial Beach, CA 91932-5000	1

	No. Copies
53. Pat Ryan OIC Naval Electronics Security Eng. Cntr. Det. 500 Silver Strand Blvd. Imperial Beach, CA 91932-5000	1
54. Robert Dreesen OIC Naval Electronics Security Eng. Cntr. Det. 500 Silver Strand Blvd. Imperial Beach, CA 91932-5000	1
55. William A. Hickey 156 Barcelona Drive Boulder, CO 80303	1

DUDLEY KNOX LIBRARY



3 2768 00347460 2